



Ph.D. DISSERTATION

Carbon Dioxide Detection Based on FET Platforms at Low Temperature

FET 플랫폼을 기반으로 한 저온에서의 이산화탄소 감지

BY

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DEPARTMENT OF ELECTRICAL AND COMPUTER ENGINEERING COLLEGE OF ENGINEERING SEOUL NATIONAL UNIVERSITY

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Carbon Dioxide Detection Based on FET Platforms at Low Temperature

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ABSTRACT

In the past few decades, carbon dioxide (CO₂) monitoring and controlling have attracted a lot of attentions. The monitoring of CO₂ outdoor helps researchers to know the change in the quality of the atmospheric air and provides important data for environment research. In the aspect of indoor air quality controlling, it is also important to detect and restrain the CO₂ concentration under a certain level, because high CO₂ concentration indoor can trigger symptoms and affect human health. By now, many efforts have been made to develop reliable CO₂ sensors with long life time, low cost, small size, low power consumption, and low working temperature. Moreover, integratable CO2 sensor is desired in order to manufacture gas arrays that are compatible with silicon CMOS technology, and extend its application in the field of portable electronic nose system.

In this dissertation, the CO₂ sensors based on FET platforms working at low temperature are investigated. Several kinds of sensing materials are applied to FET platforms, including Polyvinyl alcohol (PVA) polymer, polyethylenimine (PEI) coated single-walled carbon nanotubes (SWNT) random network, and inorganic Na⁺ ionic conducting material. All kinds of the sensing material are deposited on the FET platform by using inkjet printing process. The basic electrical and CO₂ sensing properties of these sensors are measured. The sensing mechanisms are also explained and modeled. PVA and PEI coated SWNT CO2 sensors are found to be able to detect CO₂ at room temperature (about 25°C) with the help of water vapor. The sensor with Na⁺ ionic conducting material can detect CO₂ at 160°C. all the sensors proposed in this work have much relative lower working temperature compared to typical CO₂ sensors. The FET platform makes the sensor compatible with Si CMOS technology. A floating gate is adopted in the FET component which makes the calibration of the sensor very convenient. By comparison, the sensor with Na⁺ ionic conducting material has the most stable sensing behaviors without the requirement of water vapor during the detection, and can be expected to be a promising candidate for low temperature CO₂ detection.

Keywords: carbon dioxide sensor, FET sensor, low temperature, polymer,

single-walled carbon nanotubes (SWNT), sodium ionic conducting material.

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Table 1.1. Various metal oxides for CO₂ detection and their working temperatures

Chapter 1 Introduction

1.1 Study background

1.1.1 Carbon dioxide monitoring and controlling

Carbon dioxide (CO₂) is a slightly toxic, colorless, and odorless gas with a slightly acid taste [1], [2]. It is a small but important constituent of the atmospheric air as it places an essential role in the Earth's carbon cycle. Nevertheless, CO₂ is also defined as a kind of greenhouse gases because it absorbs infrared light and can induce global climate change. The source of CO2 in air can be classified into natural and human emissions. The natural sources include ocean-atmosphere exchange, plant and animal respiration, soil respiration and decomposition, and volcanic eruptions; the human sources include industrial processes, land use changes, and fossil fuel use [3]. Both the natural and human emissions can lead variations in the concentration of the atmospheric CO₂ over space and time. However, human activities make the main contribution to the rapid concentration increase especially after the industrial revolution even though human CO₂ is a tiny component of total emissions [4]. Fig. 1.1 (a) and (b) present the atmospheric CO₂ concentration change over time recorded by Mauna Loa Observatory [5]. In Fig. 1.1 (a), the industrial revolution in the year of 1958 marked a major turning point of the CO₂ increasing rate. As shown in Fig. 1.1 (b), the concentration increased from about 315 ppm in 1958 to 407.28 ppm by November, 2018.

The monitoring of CO₂ outdoor by using gas sensors helps researchers to know the change in the quality of the atmospheric air and provides important data for environment research. In the field of indoor application, it is also necessary to develop reliable CO₂ sensors, especially home and office air qualities monitoring and controlling. A high CO₂ concentration indoor can trigger many symptoms for human, such as headaches, nausea and etc. Fig. 1.2 shows typical CO₂ levels and their effect on human beings [6]. A level of less than 1000 ppm is recommended, but if the concentration is higher than 5000 ppm, it could bring health risks. Recently, people increasingly expect portable and integratable sensors to make life more convenient. To meet the requirements for various application fields, numerous sensing materials, device structures and mechanisms of CO₂ sensing have been investigated. So far, many kinds of CO₂ sensors have been developed by research groups all over the world. Based on the sensing mechanism, they can be divided into physical and chemical ones, and the chemical sensors includes the ones rely on chemical adsorption, and electrochemical reactions [7].

The most widely used physical CO₂ sensor relies on the optical sensing principle. Fig. 1.3 presents two typical nondispersive infrared (NDIR) CO₂ sensors [8], [9]. The NDIR sensor consists of a light source, a gas chamber and a light detector. The detector receives lights from the light source through the gas chamber. As CO₂ absorbs infrared radiation at specific wavelengths, when CO₂ gas diffuses into the chamber, the light intensity reaching to the detector decreases. In Fig. 1.3 (a), the light source and detector are located at both sides of the chamber. To achieve a high regulation and fine accuracy, the gas chamber needs to be extended to increase the effective path-length of the light, which results in a quite large size of the sensor. Therefore, a parabolic mini mirror is adapted for folded or multiple reflection of the light so that sensor size can be reduced as shown in Fig. 1.3 (b) and

(c). The optical sensors have low operating temperature, long lifetime and high sensing speed. But because of their sensing mechanism, it is difficult to reduce the size of the sensors and their optical components lead to the problem of high power consumption.

In the case of CO₂ sensors based on chemical adsorption, the sensors usually consist of two electrodes connected by various sensing materials to measure the resistance or capacitance changes of the sensing materials. As metal oxides have the advantages of low cost, simplicity of their use, and large number of detectable gases [10], they have been widely investigated to detect CO₂, for example, insulator oxides like Al₂O₃, p-type semiconducting oxides like Bi₂O₃, Cr₂O₃, n-type semiconducting oxides like SnO₂, TiO₂, and composite metal oxides like CeO₂-BaCO₃-CuO, and SnO₂-La₂O₃ [11]–[17]. Table 1.1 shows a variety of metal oxides for CO_2 detection and their working temperatures [11]–[16]. At their appropriate operating temperatures, CO₂ molecules adsorb on the surface of oxides and react with them resulting in the changes in resistance or capacitance of the sensing materials. However, as the bond angle of CO₂ molecules is 180°, it makes the chemical properties of CO₂ very stable and noble, and requires high energy to support the sensing chemical reactions. Consequentially, the working temperature of this type of CO₂ sensor ranges from 300°C to 1000°C as listed in Table 1.1.

The final type is electrochemical CO₂ sensor. It can be divided into potentiometric sensor and amperometric sensor. Fig. 1.4 shows two examples of electrochemical CO₂ sensors [18], [19], where (a) is a potentiometric sensor and (b) is an amperometric sensor. The potentiometric sensor has a working electrode, a reference electrode and a solid electrolyte. On the reference electrode side of the sensor, there is a sealed air chamber, where the concentration of CO₂ will be zero or fixed at a certain level. On the working electrode side, the sensing material (sensing electrode) is exposed to target gases (CO₂ in air). With measuring the electromotive force (EMF) between the two electrodes, the change of CO₂ concentration associated with the change in EMF will be tracked. The amperometric sensor has two or three electrodes (there are two electrodes in the example of (b)). When a voltage is applied to those two electrodes, a current will flow through the electrolyte, which is measured and recorded as the sensing signal. As the

concentration of CO₂ changes, the equilibrium of the reversible electrochemical reactions at both two electrode sides will be broken and re-established. As a result, the measured current changes as a function of the CO₂ concentration. This type of sensor still requires high operating temperature (above 300°C). Moreover, they are usually discrete devices with large size and it is very difficult to integrate them with CMOS technology.



Fig. 1.1 Change in concentration of CO₂ in air over time [5]. (a) CO₂ concentration record from the year of 1700 to present. (b) CO₂ concentration record from 1958 to present.



How does CO₂ affect the human body?

Fig 1.2 Typical CO₂ levels indoor and their effects on human beings [6].



Fig. 1.3 The schematic diagram of optical CO₂ sensor with a straight light path (a) [8], a folded reflection (b) and a multiple reflection (c) [9]. The PD in the figure refers to the photodiode.

Sensing material	Classification	Working temperature	Reference
Al ₂ O ₃	Insulator	450°C	[11]
Bi ₂ O ₃	p-type semiconductor	450°C	[11]
Cr ₂ O ₃	p-type semiconductor	450°C	[11]
CuO	p-type semiconductor	450°C	[11]
NiO	p-type semiconductor	450°C	[11]
CdO	n-type semiconductor	450°C	[11]
Fe ₂ O ₃	n-type semiconductor	450°C	[11]
TiO ₂	n-type semiconductor	450°C	[11]
ZnO	n-type semiconductor	450°C	[11]
SnO ₂	n-type semiconductor	350°C	[12]
WO ₃ -loaded TiO ₂	composite	600°C	[13]
BaTiO ₃ (CeO ₂ /ZrO ₂ /CaCO ₃ /Nd ₂ O ₃ /La ₂ O ₃ /Fe ₂ O ₃)	composite	300-640°C	[14]
CeO ₂ with BaCO ₃ , CuO	composite	550-600°C	[15]
La-coated SnO ₂	composite	400°C	[16]

Table 1.1. Various metal oxides for CO₂ detection and their working temperatures [11]–[16].



Fig. 1.4 Examples of electrochemical CO₂ sensors. (a) Potentiometric sensor [18].

(b) Amperometric sensor [19].

1.1.2 Gas sensors based on FET platforms

To achieve the full potential of sensing materials, different kinds of sensor platforms are designed, some of which have been discussed in the above section. Recently, there is an increasing interest in field-effect-transistor (FET)-type sensors because they can be fabricated with standard CMOS technology used to make integrated circuits [20]. In this case, it is possible to reduce the size of sensors, lower the power consumption, and fabricate sensors in a reproducible way [21]–[23].

In 1975, Lundström et al. proposed the first Pd-gate FET gas sensor for H₂ detection as shown in Fig. 1.5 [24], [25]. This type of sensor has a Pd sensing gate. During the detection of H₂ gas, the gas molecules are adsorbed and can decompose into atoms at the outside surface of Pd. Thanks to the small size of H atoms, they can penetrate through the Pd gate and reach to the interface between Pd and gate oxide. Those H atoms will form a dipole layer at the interface resulting in a change in the threshold voltage (V_{th}) of the FET shown as Fig. 1.5. The proposed Pd-gate sensor opened the wide applications of FET to the field of sensor platform. However, because its sensing behaviors require the size of target gas molecules small enough

to penetrate through the sensing gate, the usage of this type of sensor for other target gases were limited.

In order to greatly expand the number of gas species that can be detected by FET sensors, Janata proposed a FET sensor platform with an air gap named suspended gate (SG) FET shown as Fig. 1.6 [25], [26]. It has a suspended gate bonded to the substrate. An air gap is generated between the suspended gate and gate oxide. The sensing material is attached to the gate to absorb the target gas. As the capacitance between the gate and channel is changed by the target gas, the $V_{\rm th}$ is changed. The air gap allows gas molecules access to the sensing material regardless of the size. However, the gate oxide could be contaminated very easily, which will induce considerable noise and fluctuation of V_{th} and sensing signals. Therefore, a capacitively-controlled FET (CCFET) with a floating gate was proposed by researchers, which is shown in Fig. 1.7 [27]. The CCFET with a floating gate dramatically improves the sensing performance of sensors, but it complexed the fabrication of sensors to cover the suspended gate with sensing material and bond the gate to the substrates. To simplify the fabrication process and

make the device more compatible with standard CMOS technology, our group proposed a FET sensor platform having horizontal floating gate and control gate. Fig 1.8 shows the sensor with horizontal floating gate and control gate investigated in our previous work [28]. The platform was fabricated with standard CMOS technology. The sensing material was formed at the final step after the fabrication of the platform.



Fig. 1.5 Lundström FET H₂ sensor. (a) Shematic of the sensor [25]. (b) The V_{th} of

the FET is changed by H_2 gas.



Fig. 1.6 Suspended gate (SG) FET sensor with an air gap [25].

alumina substrate				
gas sensitive layer	air gap			
oating gate				
(passivation opened)				
Canacitanas wall				
Capacitance well				
Substrate (p-Si)				
	readout FE			

Fig. 1.7 Capacitively-controlled (CC) FET sensor with a floating gate [27].



Fig. 1.8 FET sensor platform having a horizontal floating gate and control gate [28].(a) The SEM image of the sensor. (b) The cross sectional view cut along line A-A' in (a).

1.2 Purpose of research

Even though a lot of efforts have been made to lower the working temperature of the chemical and electrochemical CO2 sensors, further more research is still required for achieving a stable FET CO₂ sensor having low power consumption and low working temperature. In this work, we combined various novel sensing materials with FET platform for CO₂ detection to reduce the working temperature. Carbon based sensing material and PVA polymer are able to detect CO₂ at room temperature. Whereas, the sensing mechanism seriously relays on the help of moisture (water vapor), which limits the application of the sensor. Finally, a sodium ionic conducting materials is applied to the platform. As known that sodium ions have high mobility and can induce unacceptable instabilities in MOSFET operation, so they should be avoided in CMOS technology. If the ions inside the sensing material penetrate into the FET platform, they will cause serious problem of stability of the sensor. Fortunately, with the protection of a selfassembled monolayer - APTES, sodium ions can be prevented from leaking into the substrate.

1.3 Dissertation outline

In this work, CO₂ sensors based on FET type platform with horizontal floating gate and control gate working at low temperature are proposed and investigated. Chapter 2 introduces the detailed fabrication flow of the FET platform and the formation of sensing materials. Chapter 3 shows the measurement results and discussion about the electrical and CO₂ sensing properties of the sensors with various sensing materials. In Chapter 4, the sensing mechanisms of the sensors with the carbon based material and the sodium ionic conducting material are explained and modeled. Finally, Chapter 5 concludes this work with a summary.
Chapter 2

Device structure and fabrication

2.1 FET platform structure and fabrication

The FET platform used in this work is shown in Fig. 2.1. Fig. 2.1 (a) is the SEM top view of sensor platform, (b) and (c) are the schematic cross sectional views cut along A-A' and B-B' in (a), respectively. As shown in Fig. 2.1, the floating gate (FG) and control gate (CG) are formed horizontally. An interdigitated pattern is adopted to guarantee a promising coupling ratio between the two gates. Note that, an SU-8 passivation layer covers the whole substrate except the FG-CG area (marked out in Fig. 2.1 (a)) and electrode contact pads. Because the sensing material will be deposited in the final step, the SU-8 protects the active regions of FET from unwanted contaminations and only expose the interdigitated FG-CG region to the sensing material. To fabricate the FET substrate, 5 masks are needed. The main process flow is shown in Fig. 2.2.

The process starts with a 6-inch n-type (100) Si water. Firstly, the wafer is

cleaned using RCA cleaning process to remove oxides and all particles on the wafer. After cleaning, 10-nm SiO₂ and 150-nm Si₃N₄ are formed through dry oxidation and low pressure chemical vapor deposition (LPCVD) processes, respectively. With the first mask, the active device regions are defined by photolithography process. The silicon substrate with Si₃N₄/SiO₂ mask patterned by dry etching shown as Fig. 2.2 (a). Through 2-hour wet oxidation, a thick field oxide with a thickness of about 550 nm is grown to insulate transistors (Fig. 2.2 (b)). Because Si₃N₄ is resistant to oxidation, thick oxide only grows within the regions without Si₃N₄, which is called as Local Oxidation of Silicon (LOCOS) process. Then the SiO₂/Si₃N₄ mask is removed by wet etching (H₃PO₄ for Si₃N₄ and HF for SiO₂) During LOCOS process, the Si₃N₄ could be oxidized by H₂O and generates NH₃ gas. The NH₃ gas can diffuse to the interface of Si and SiO₂, reacts with Si and produces Si₃N₄, so called white ribbon [29]. To remove the white ribbon, a 35-nmthick oxide is grown by dry oxidation process, and a back-etch is conducted leaving 10nm oxide (sacrificial oxide) above the active regions. Then a punch-though and a buried channel implantations are processed. After removing the sacrificial oxide by HF solution, a 10-nm-thick SiO₂ is produced by dry oxidation to serve as the gate oxide. A 200-nm-thick in-situ phosphorous doped Poly-Si layer is deposited and pattern using the second mask to form the FG. Stacked ONO insulator layers consisting of SiO₂ (10 nm) / Si₃N₄ (20 nm) /SiO₂ (10 nm) cover the whole substrate to prevent contamination of the platform from the final deposition step of the sensing material and the penetration of moisture after fabricating the device. The first layer of SiO₂ is thermally grown on the wafer, and the Si₃N₄ and the second SiO₂ are deposited by LPCVD and methanol to olefins (MTO) processes. Then the source and drain are implanted. To form the contact hole, the third mask is used, followed by the electrode metal deposition and lift-off process (Fig. 2.2 (c)). After defining the contact holes, stacked layers of Ti (20 nm) / TiN (30 nm)/ Au (30 nm) are formed consecutively by sputtering to serve as the CG, source, and drain electrodes. The electrodes are patterned by using the forth mask and this step is shown in Fig. 2.2 (d). The final step of FET substrate fabrication is SU-8 passivation layer deposition. In this step, a thick layer of SU-8 is deposited and patterned by spin coating and photolithography (Fig. 2.2 (e)). In this way, only the FG-CG area (marked in Fig. 2.1 (a)) and electrode contact pads are exposed to the air. Fig. 2.2 (f) shows the FET substrate covered by sensing material. Finally, several sensing materials are deposited on the fabricated substrate and are investigated for CO₂ detection at relative low temperature in this work.



Fig. 2.1. (a) SEM top view of sensor platform. (b) Schematic cross sectional view

cut along A-A'. (c) Schematic cross sectional view cut along B-B'.



Fig. 2.2 The main fabrication flow of the FET substrate. (a) Silicon wafer with patterned Si₃N₄/SiO₂. (b) The FG is patterned. (c) ONO stack is deposited to cover the whole substrate. (d) Electrodes are patterned. (e) The SU-8 layer is deposited and patterned to expose the interdigitated FG-CG and electrode pads only. (f) The sensor with sensing material.

2.2 Sensing materials deposition

In this work, all the sensing materials were deposited on the sensor FET substrates by inkjet printing process. The instrument for inkjet printing used in this work is Omni Jet 100. To reduce the working temperature of the CO₂ sensor, various kinds of sensing materials were investigated in this dissertation, including organic polymers, carbon based nanomaterials, and inorganic ionic conducting materials. The following sections will provide introduction to the sensing materials used in this work and their deposition processes.

2.2.1 Organic polymer based sensing material

Polymer materials have attracted increasing attentions recently because they can be fabricated by low-cost and simple processes, and require low gas sensing temperature. In this work, Polyvinyl alcohol (PVA) is used to detect CO₂, based on the reactions between CO₂ and –OH (with the help of water) at room temperature (25°C). The PVA powders with an average mole weight (Mw) of 13000-23000 are purchased from Sigma-Aldrich (USA). As PVA is soluble in hot water, 0.2 g of purchased PVA powders is dissolved in 30 mL of mixture of deionized (DI) water and DMOS (4:1 in volume). To make an appropriate ink solution, firstly, PVA powders are soaked in the solvent at 25°C with stirring for 1h by using Hotplate & Magnetic stirrers (MTOPS production). In this process, the white particles turn into transparent. After that, the solid-liquid mixture is allowed to stand for 12 hours at 25°C (swelling). Then we increase the temperature to 95 °C and stir the mixture for 14 hours at 95°C for sufficiently solving PVA particles. Finally, the solution is cooled at 25°C, and filtered with 0.2 µm syringe filter. The chemical formula of PVA and the finally obtained ink solution is shown in Fig. 2.3. The as-prepared PVA ink is injected into 4 mL ink cartridge for printing. Fig. 2.4 (a) shows the PVA ink printed on the surface of FET sensor substrate at 25°C and Fig. 2.4 (b) is the capture of ink droplet. After printing, the sensor is cooled in air for 12 hours and stored for measurement.



Fig. 2.3 PVA ink obtained by dissolving PVA powders in the mixture of DI water and DMOS (4:1 in volume).



Fig. 2.4. (a) Printed PVA ink on the FET sensor substrate. (b) Capture of the ink flow printed from the ink cartridge.

2.2.2 Carbon based sensing material

Besides polymers, carbon based sensing materials, like CNT and graphene, have also attracted many attentions because they can detect CO₂ even at room temperature [30]. In this section, a sensing material of polyethylenimine (PEI) coated single-walled carbon nanotubes (SWNTs) is investigated for the detection of CO₂ at room temperature (25°C). The layer-by-layer PEI-coated SWNT (PEI-SWNT) sensing materials are formed by inkjet printing.

Semiconducting SWNT ink (1mg 98%) is purchased from NanoIntrgris (Canada) and printed on the platforms at 50°C without further processing. Then the device is annealed under vacuum at 250°C for 3 hours to evaporate the solvent. The next step is to print the PEI to cover the SWNT random networks. Since ink having a viscosity of 1 to 10 cps is suitable for inkjet printing [31], when producing PEI ink, a Wt. 50% branched PEI aqueous solution (number average molecular weight 1200) purchased from Sigma-Aldrich (USA) is diluted to 10⁻³ mol/L with DI water to reduce the viscosity of the solution. After printing the PEI, the sensor is heated at 60°C for 2 hours and then cooled in air for 1 hour. Fig. 2.5 presents the microscopic images and schematics of the printed sensing materials. Fig. 2.5 (a) shows the platform used for the sensors having carbon based sensing materials. Fig. 2.5 (b) and (c) show the images of printed pure SWNT random network and PEI-SWNT, respectively. Coffee ring effect is rarely observed in the images indicating the printing condition of the SWNTs is reasonable. Unlike the pure SWNTs which concentrate densely in the center of the printed layer, the PEI molecules disperse the nanotubes and make their distribution more uniform. Fig. 2.5 (e) and (f) show the schematic 2D cross sectional view of the sensor with pure SNWT and PEI-SWNT cut alone line A-A' in Fig. 2.5 (a) which explaining how the PEI disperses the nanotubes.



Fig. 2.5. (a) the platform used for the sensors having carbon based sensing materials.(b) and (c) show the images of printed pure SWNT random network and PEI-SWNT.(e) and (f) show the schematic 2D cross sectional view of the sensors with pureSNWT and PEI-SWNT cut alone line A-A' in (a), illustrating the dispersion of the nanotubes by PEI.

2.2.3 Sodium ionic conducting sensing material

Alkali carbonates and related ionic conducting materials are widely used in the field of CO₂ detection based on electrochemistry, especially materials containing sodium ions. However, it is required to avoid mobile ions like Na⁺ ions as much as possible in the CMOS fabrication. As a result, most of the electrochemical CO₂ sensors are discrete devices and other planar ones are usually formed on insulate substrate (like, Al₂O₃ substrate). In this work, a sensing material full of Na⁺ ions, the compound of Na₂CO₃ and NaNO₂, are applied for CO₂ detection. Experiment shows if the sensing material is directly deposited on the surface of the FET sensor substrate, the Na⁺ ions inside the sensing material will penetrate very easily into the oxide and induce large leakage currents. Therefore, before the deposition of the sensing layer, a self-assembled monolayer (SAM) of (3-Aminopropyl) triethoxysilane (APTES), of which the linear formula is H₂N(CH₂)₃Si(OC₂H₅)₃, is formed on the exposed interdigitated FG and CG region by using simple dipping method. The measurement results indicated that it can effectively prevent the Na⁺ ions from diffusing through the insulator stack and even the thick isolation oxide.

Fig. 2.6 shows the process flow of forming the SAM layer. To conform the assembling of APTES on the substrate, the contact angles after each steps were recorded and presented in Fig. 2.6. Fig. 2.6 (a) left illustrates the initial substrate (covered by SiO₂) and the water contact angle. Firstly, the platform is illuminated by UV to create a large amount of –OH groups on the oxide in the exposed region of interdigitated FG and CG as shown in Fig. 2.6 (b). Because the -OH is more hydrophilic than SiO₂, the contact angle in the right side of Fig. 2.6 (b) is getting much smaller and close to zero compared to that in (a). Then the substrate is immersed in 1% APETS solution (dissolved in 99.99% Ethanol) for 30min. After baking at 120 °C for 10min, the APTES monolayer assembles itself on the oxide surface of the ONO stack in the FET platform as shown in Fig. 2.6 (c). The contact angle is found to get larger again, which certifies that the APTES layer successfully assembles on the substrate.

For preparing the ink of sensing material, powders of Na₂CO₃ and NaNO₂ with a molar ratio of 1:3 were dissolved in DI water. Both chemicals were purchased from Sigma-Aldrich (USA) without further purification. After inkjet printing, a 2hour annealing process at 170°C under vacuum condition was conducted to fully evaporate the water in the printed ink and form the porous Na₂CO₃ and NaNO₂ sensing layer (an average pore size of about 500 nm). Fig. 2.7 (a) shows the SEM image of the sensor with the sensing material and (b) shows the magnified porous sensing material.



Fig. 2.6. (a) The initial substrate (SiO₂ covered silicon substrate) and its water contact angle. (b) The substrate illuminated by UV and the contact angle. A large amount of –OH groups are generated on the surface of oxide. The contact angle is getting smaller. (c) The substrate with assembled APTES monolayer. The contact angle is getting larger again indicating the presence of SAM layer.



Fig. 2.7 (a) The SEM image of the sensor with the sensing material. (b) Magnified

porous sensing material.

2.3 Gas sensing measurement system

Experiment found that water vapor plays a very important role when using PVA and PEI-SWNT to detect CO₂ at 25°C (will be explained in Chapter 3 in detail). Thus both dry and wet CO₂ detection are investigated for them. In the measurement of sensors with Na⁺ ionic conducting material, only dry gases are used. As discussed in literature [32], ambient water vapor may affect the detection of CO₂ by forming additional CO₃²⁻ and/or HCO₃⁻. Because the working temperature of this sensor is kept around 160°C, only the study of dry CO₂ sensing is focused on. For wet CO₂ detection, a bubbler is involved in the gas sensing measurement system, which is illustrated in Fig. 2.8. The MFC in the figure refers to the mass flow controller. The CO₂ gas samples are prepared by mixing 2000-ppm CO₂ diluted in N₂ with dry synthetic air (20 vol. % of O₂ and 80 vol. % of N₂). Reference gas 1 will flow through the bubbler to bring water vapor into the mixing chamber. By controlling the flow of reference gas 1, the relative humidity (RH) can be tuned. With fixing the total flow of reference gas1, reference gas 2 and CO₂ gas, the concentration of CO₂ and the RH level can be regulated well by changing the flow of these three

gases. Fig 2.9 shows the gas sensing measurement setup for dry CO₂ detection. The sensing characteristics are tested by switching between the sample target gas and the reference gas (dry air or pure N₂). Electrical measurements are carried out by using an Agilent B1500A including Waveform Generator/Fast Measurement Unit (WGFMU) pulse measurement module.



Fig. 2.8 Setup of the gas sensing measurement system for wet CO₂ detection.



Fig. 2.9 Setup of the gas sensing measurement system for dry CO_2 detection.

Chapter 3

Measurement results

3.1 PVA CO₂ sensor

In this section, the basic electrical and CO₂ sensing characteristics of the PVA sensor are investigated at 25°C. Fig. 3.1 plots the DC IV curve of the PVA sensor. Fig. 3.2 shows the sensing performance of the sensor for 400 ppm CO₂ at 25°C. As 400 ppm of CO₂ gas sample blows into the sensor for 5 min, the absolute drain current $|I_D|$ of the sensor decreases, and when the reference gas replaces CO₂ gas, the $|I_D|$ increases. The response of the sensor to CO₂ gas is defined as

$$response = [(|I_{D_B}| - |I_{D_G}|)/|I_{D_B}|] \times 100\%$$
(1)

where I_{D_B} and I_{D_G} represent the drain currents of the sensor exposed to the reference gas and the target gas mixture, respectively. We define the response time (*t*_{RES}) as the rise time of $|I_D|$ to 90% of its maximum value, and the recovery time (*t*_{REC}) as the fall time to 10% of the difference between the maximum and reference currents. After calculation, the *response*, *t*_{RES}, and *t*_{REC} of the PVA sensor are 6%,

80 s and 60 s, respectively, for 400 ppm of CO₂ at 25°C.

Next, the PVA sensor is stored in air for two weeks, and the sensing performance is measured again as shown in Fig. 3.3. The measurement condition is the same with that of Fig. 3.2. During the response period, 400 ppm of CO₂ blows into sensor for 5 min and then reference gas replaces the CO₂ gas sample to refresh the sensor. It is obvious that the sensor cannot reach saturation current within 5 min. Moreover, the fluctuation of the drain current is getting larger compared to that of the results in Fig. 3.2. It illustrates that the sensor is degraded during storage in air.

To figure out the reason for the degradation, the sensor was heated at 180°C for 1 hour and then the sensing properties of the sensor for 400 ppm of CO₂ was measured again and shown in Fig. 3.4. This time, the sensor didn't respond to CO₂ any more. The reason seems to be that the water inside the PVA sensing material was fully evaporated after the 1-hour heating treatment. During the formation of the PVA sensing material, the device was just cooled and dried in air at room temperature. As the PVA ink for printing is composed of PVA, DI water and DMSO, water molecules may partially remain inside the sensing material even though the

DMSO is very easy to evaporate. According to literature [33], [34], water molecules bonds to the -OH groups of PVA through hydrogen bonding. These water molecules will react with CO₂ and induces the change in threshold voltage resulting in the decreases of the drain current. This process is illustrated in Fig. 3.5. It indicates that the water plays a principal role in the detection of CO₂ at room temperature when using PVA as the sensing material. Then wet air is used to blow into the sensor for 3 h and the CO₂ sensing performance was measured again. There was still no response of the sensor to CO₂ gas sample. According to literature [35]-[37], PVA can be decomposed by raising up the temperature and generate the production of water. In conclusion, the PVA sensor requires water vapor during the CO₂ detection at room temperature and has short life time, which limits its practical application in gas detection.



Fig. 3.1 Double-sweep DC IV curve of the PVA sensor at 25°C.



Fig. 3.2 Sensing performance of the PVA sensor for 400-ppm CO₂ at 25°C.



Fig. 3.3 Degradation of the PVA CO₂ sensor after two weeks of storage in air.



Fig. 3.4 The PVA sensor didn't respond to CO₂ gas after heated at 180°C for 1 hour.



Fig.3.5 Water molecules bond with the –OH groups of PVA molecules and play a principal role in the detection of CO₂ (according to [33]).

3.2 PEI-SWNT CO₂ sensor

In this section, PEI coated SWNT sensing material is used for CO₂ detection at 25°C. SWNTs have different conducting types depending on their lattice structures as shown in Fig. 3.6 [38]. In this work, p-type semiconducting SWNT is used. Branched PEI covers the SWNT for reducing the hysteresis.

Fig. 3.7 shows double-sweep DC IV curves of the SWNT sensor and the PEI-SWNT sensor at 25°C. By comparison, the PEI-SWNT sensor has much smaller I-V hysteresis than the SWNT sensor with the help of PEI coating. According to literature [39], as the SWNTs contact silicon dioxide, a large amount of traps will be generated at the interface and induce a significant I-V hysteresis due to charge trapping and detrapping. Whereas, by coating the SWNT with PEI, the nanotubes will be dispersed by PEI. The schematic of PEI-bonded CNT is shown in Fig. 3.8 [40]. The PEI coating reduces the contact of SWNT network with the oxide, resulting in less interface traps. Therefore, the hysteresis is reduced.



Fig. 3.6 Various types of CNT nanotubes [38].



Fig. 3.7 Double-sweep DC IV curves of the SWNT sensor and the PEI-SWNT sensor at room temperature. The I-V hysteresis of the PEI-SWNT sensor is smaller than that of the SWNT sensor.



Fig. 3.8 Schematic of PEI-bonded CNT [40].

The FET sensor substrate used in this work can be electrically programmed because of the FG structure, which makes the calibration of the sensor possible. Fig. 3.9 (a) and (b) show the double-sweep pulsed IV (PIV) curves of the programmed SWNT sensor and PEI-SWNT sensor, respectively. The $V_{th}s$ of both sensors are shifted to positive direction after programming compared to the results in Fig. 3.7. The inset shows pulse scheme for PIV. Pulsed gate biasing limits the time of charge trapping and detrapping and reduces I-V hysteresis. In Fig. 3.9, the I-V hysteresis of the PEI-SWNT sensor is removed by pulse measurement but the I-V hysteresis of the SWNT sensor still exists. By coating SWNT network with PEI and applying the pulse measurement, the I-V hysteresis in the sensor is nearly eliminated.

Fig. 3.10 (a) and (b) show the dry CO₂ sensing properties of the PEI-SWNT

sensor measured by applying DC biases at 25°C after one day and 2 weeks, respectively, after PEI coated SWNTs are deposited on the sensor platform. In Fig. 3.10 (a), the drain current decreases when the sensor is exposed to CO₂ target gas sample. However, after two weeks (Fig. 3.10 (b)), the sensor has barely no response to dry CO₂ gases. This may be attributed to the effect of moisture on the CO₂ detection. It seems that the water left in the sensing material is fully evaporated within two weeks and the response to CO₂ is degraded. Therefore, it is necessary to investigate the effect of moisture on CO₂ gas detection using PEI-SWNT sensor.

Fig. 3.11 shows wet CO₂ sensing properties of the PEI-SWNT sensor with the sensing material formed two weeks before the measurement. DC biases are applied to the sensor. Before measuring, we humidify the sensing material by blowing humid air into the sensor for 3 hours. During the wet CO₂ measurement, the relative humidity (RH) of the gas is set to be 30%. With the help of water vapor within the target gas sample, the drain current decreases with the increase of CO₂ concentration again. It indicates that the PEI-SWNT sensor requires moisture for the detection of CO₂ at room temperature. Both CO₂ gas and water vapor involve

in the reaction with the sensing material and decrease the drain current.

As shown in Figs. 3.10 and 3.11, there is drift in the drain current over time. It has a significant impact on the accuracy of CO₂ detection. Hence, a pulse scheme for transient measurement is introduced to obtain reliable measurement results without drift. The pulse scheme is shown in Fig. 3.12 (a). An appropriate pre-bias $(V_{\rm pb})$ and read bias $(V_{\rm r})$ are applied sequentially to the CG. Note that when $V_{\rm pb}$ is applied to the CG, V_{DS} is set to 0 V simultaneously to remove unwanted power consumption. In read biasing period, both V_r and V_{DS} are synchronized and have finite biases. During the read period, the drain current of the sensor will be read out and recorded as the sensing signal. Here, the width of V_{pb} pulse (t_w) and V_r pulse (t_r) are set to 1 s and 50 µs, respectively. Fig. 3.12 (b) shows wet CO₂ (30% RH) detection characteristics of the PEI-SWNT sensor obtained by applying the pulse scheme at room temperature. The drift is removed by the pulse measurement method. In Fig. 3.12, our sensor shows a *response* of 16%, a t_{RES} of 81 s and a t_{REC} of 202 s for 2000 ppm of CO₂ at 25°C.

In this section, the measurement results show that the PEI-SWNT sensor can

detect CO₂ at room temperature with the help of water vapor. The current drift was removed by using pulse measurement method and the sensor presented short response and recovery speeds, and reasonable response amplitude. However, the PEI-SWNT needs water vapor for CO₂ detection, which may limit the application of the sensor in the real gas detection.



Fig. 3.9 Double-sweep PIV curves of the SWNT sensor (a) and the PEI-SWNT sensor (b) at 25°C after programming.



Fig. 3.10 Dry CO₂ sensing properties of the PEI-SWNT sensor measured by applying DC biases at 25°C after one day (a) or two weeks (b) after the sensing material is deposited.



Fig. 3.11 Wet CO₂ detection characteristics of the PEI-SWNT sensor measured by applying DC bias at 25°C.



Fig. 3.12 (a) Voltage pulse scheme for measuring sensing characteristics. (b) Wet CO₂ detection characteristics of the PEI-SWNT sensor measured by applying the voltage pulse at 25°C.

3.3 Na⁺ ionic conducting CO₂ sensor

In sections 3.1 and 3.2, CO₂ sensors based on PVA and PEI-SWNT are investigated at room temperature. Both of them need water vapor to react with CO₂ during the detection. In this section a sensing material of Na₂CO₃ and NaNO₂ compound is used for CO₂ detection. The working temperature is around 160°C. Between the substrate and the sensing material, an APTES SAM layer is formed. Without this APTES layer, the Na⁺ ions will penetrate into the oxide very easily during heating process and induce large leakage current. In section 3.3.1, the function of APTES is addressed. In section 3.3.2, the sensing performance of the Na⁺ ionic conducting CO₂ sensor is measured. Finally, the sensor is programmed and the sensing properties of programmed sensor is characterized in section 3.3.3.
3.3.1 APTES SAM ion-blocking layer

As described above, APTES SAM was formed on the oxide surface of the ONO stack in the exposed interdigitated FG-CG region to prevent the penetration of Na⁺ ions. A comparison of electrical characteristics between the devices with and without APTES SAM is carried out to demonstrate the ion-blocking capability of the APTES. Fig. 3.13 (a) and (b) plot the I_D - V_{CGS} curves of the sensors with and without the APTES ion-blocking layer, respectively, as a parameter of temperature (20°C and 160°C). The insets in both figures show the CG leakage currents (I_G). When the sensing layer directly contacts with the ONO passivation layer covering the FG, the Na⁺ ions contained in the sensing material penetrate through the passivation layer during annealing process. It seems that the diffusion of the Na⁺ ions makes many leakage paths through the insulator layers. The inset in Fig. 3.13 (a) shows very high CG leakage current (~10 nA) even at 20°C. Fig. 3.14 illustrates the penetration of Na⁺ ions (Fig. 3.14 (a)) and the protective effects of the APTES monolayer (Fig. 3.14 (b)). In Fig. 3.13, the drain current exhibits significant fluctuation and quite poor modulation with the change of the CG bias. The

penetrated ions create paths from the gate to the source resulting in the high gate leakage current. At the same time, the large number positive Na⁺ ions inside the oxide near the channel can attract additional electrons making the large off state current and give rise to more scattering. Conversely, the APTES SAM formed on top of the passivation layer effectively blocks the diffusion of the Na⁺ ions so that the gate leakage is negligible (less than 10^{-13} A) and reasonable *I*_D-*V*_{CGS} curves are obtained as shown in Fig. 3.13 (b).

An APTES molecule consists of a head group, a tail and a functional group (-NH₂ groups) [41]. The "head group" assemble itself on the surface of the ONO stack through the chemical reaction with the -OH groups. The tail and functional group are located far from the stack. As the schematic shows in Fig. 3.15, the -NH₂ groups will capture Na⁺ ions and form a complex of APTES-Na⁺ [42]–[45]. In this way, the mono APTES layer kept Na⁺ ions away from the ONO stack.



Fig. 3.13 I_{D} - V_{CGS} characteristics showing Na⁺ ion-blocking capability of APTES SAM. Figures (a) and (b) show the I_{D} - V_{CGS} curves of the sensors with and without the APTES ion-blocking layer, respectively, as a parameter of measurement temperature (20°C and 160°C). The insets plot the I_{G} - V_{CGS} curves showing the control-gate leakage current.



Fig. 3.14 (a) The penetration of Na ions. (b) The protective effects of the APTES monolayer.



Fig. 3.15 The $-NH_2$ functional groups capture Na^+ ions and form a complex of APTES-Na⁺ to prevent the penetration of Na⁺ ions.

Fig. 3.16 (a) and (b) shows the *I*_D-*V*_{CGS} curves of three FET sensors having three different materials on the exposed interdigitated FG and CG: nothing (air) (Fig. 3.16 (c)), APTES only (Fig. 3.16 (d)), and both APTES and sensing materials (Fig. 3.16 (e)) at different temperatures. Note the three sensors have the same geometries and structure, and were fabricated on the same silicon substrate. The device having both APTES and sensing material is working properly as a normal *p*MOSFET with negligible gate leakage current at both 20°C and 160°C. However, the FET sensor with air or APTES only cannot be turned on even at a CG bias of -6 V no matter at 20°C or 160°C, because the capacitive coupling between the CG and the FG is too low compared to that between the FG and the channel. The results in Fig. 3.13 and Fig. 3.16 conclude that the sensing layer enhances the capacitive coupling ratio between CG and FG. In addition, the APTES ion-blocking layer effectively prevents the Na⁺ ion leakage and will not affect the electrical characteristics of the *p*MOSFET because its thickness is only about 1 nm [46]–[49]. It makes the Na⁺-ion-conducting solid electrolyte compatible with the FET-type sensor platform.



Fig. 3.16. $I_{\rm D}$ - $V_{\rm CGS}$ curves of three FET platforms having different materials (nothing (air), APTES SAM only, both APTES SAM and sensing material) on the exposed interdigitated FG and CG at measurement temperatures of 20°C (a) and 160°C (b). The insets are the $I_{\rm G}$ - $V_{\rm CGS}$ curves.

Except APTES, two more SAM materials, n-octadecyltrichlorosilane (ODTS) and 1H,1H,2H,2H-Perfluorooctyltriethoxysilane (F-OTS) are also investigated for comparison. After forming the two SAM layers separately on two FET sensor substrates, the Na⁺-ion-conducting material (Na₂CO₃ and NaNO₂ with a molar ratio of 1:3) are printed on both two substrates using the same process described in Chapter 2. The formulas of ODTS and F-OTS are shown in Fig. 3.17. The functional groups of APTES, ODTS and F-OTS are -NH2, -CH3, and -CF3, respectively. Fig. 3.18 plots the ID-VG and IG-VG curves of sensors with ODTS and F-OTS at 20°C. Large leakage currents are found in both ODTS and F-OTS sensors. Even though ODTS and F-OTS can also assemble on the surface of the substrates to form monolayers between the sensing material and the FET substrates, the Na+ ions still can easily penetrate into the oxide resulting in large leakage current. It indicates that the specie of functional groups determines the ion preventive capability of the SAM layer. In a word, Only the APTES of the investigated three SAM materials reacts with Na⁺ ions producing APTES-Na⁺ complexes and presents an outstanding ion blocking effect.



Fig. 3.17 The chemical formulas of ODTS and F-OTS. The functional groups of

ODTS and F-OTS are -CH3, and -CF3, respectively.



Fig. 3.18 I-V curves of sensors with ODTS and F-OTS at 20°C. Large leakage currents are found in both ODTS and F-OTS sensors.

3.3.2 Gas sensing performance

Fig. 3.19 (a) shows the CO₂ sensing performance of the proposed sensor with N₂ as the reference gas and (b) shows the track of gate leakage current. The operating temperature here is 160°C for good stability of the sensor, relative low heat power consumption and relative high ionic conductivity [50]. Constant biases are applied to the CG and drain electrodes to keep a certain absolute drain current level ($|I_D|$). The $|I_D|$ is changed and recorded as the sensing signal by changing the ambient gas. First, the sensor is held in a test chamber filled with N₂. When the $|I_D|$ of the sensor saturates after a-few-minute drift, a target gas consisting of 180 ppm of CO₂ and dry synthetic air is provided to the chamber. The $|I_D|$ is increased by the target gas.

According to Fig. 3.19, *response*=133%, t_{RES} =550 s and t_{REC} =820 s for 180 ppm of CO₂ at 160°C. A fluctuation in the $|I_D|$ is observed when the sensor is starting to approach saturation. It may result from the physical and chemical processes taking place at the gas/gate metal/Na⁺-ion-conducting material three-phase-boundary (TPB) [51].



Fig. 3.19 CO₂ sensing performance of the proposed sensor with N₂ as the reference gas at 160°C. The increase of CO₂ concentration induces the increase of the drain current $|I_D|$.

3.3.3 Programming of the FET sensor platform

Due to the FG of our FET-type sensor platform, the sensor can be programmed or erased just like a common memory device. The V_{th} of the sensor can be controlled by the programming and erasing conditions (programming/erasing voltages and time), which is beneficial to the calibration and the adaptation of the sensor to meet different operating requirements [52]. In Fig. 3.20, the sensor is programed by the condition of V_G =15 V at V_D = V_S =0 V for 10 s at 150°C and the V_{th} is shift to the positive direction by about 5 V. In this way, a reasonable current can be obtained by applying a very small CG bias or even zero CG bias.

The $I_{\rm D}$ - $V_{\rm CGS}$ curves of the sensor before and after programing are plotted in Fig. 3.20 (a). The $|I_{\rm D}|$ transient curve of the sensor in N₂ ambient after programing is shown in Fig. 3.20 (b), which indicates stability of the sensor. Fig. 3.21 (a) shows the sensing performance of the programed sensor for 500 ppm CO₂ with N₂ reference gas at 150°C. Note that $V_{\rm CGS}=0$ V during the measurement, and the MOSFET works in the linear region according to the $I_{\rm D}$ - $V_{\rm CGS}$ curve in Fig. 3.20. Fig. 3.21 (b) shows $\Delta I_{\rm D}$ ($\Delta I_{\rm D}=|I_{\rm D_-G}|-|I_{\rm D_-B}|$) as the function of CO₂ concentration at 150°C after programming. Here, the reference gas is synthetic air in place of N₂. To remove the influence of O₂ on the sensing performance, we keep a constant proportion of the O₂ in both the reference gas and the target gas sample by balancing the concentration of CO₂ with N₂. The ΔI_D increases with the increase of CO₂ concentration.



Fig. 3.20 (a) The *I-V* curves of the sensor before and after programing. (b) I_D

transient curve of the sensor in N2 ambience after programing.



Fig. 3.21 (a) Sensing performance of the programed sensor for 500 ppm CO₂ with N₂ reference gas at 150°C. (b) ΔI_D as the function of CO₂ concentration after programming the sensor. $\Delta I_D = |I_D_G| - |I_D_B|$.

Chapter 4

Device sensing mechanism

4.1 Sensing mechanism of PEI-SWNT sensor

By comparison, the sensors with Na⁺ ionic conducting material and PEI-SWNT present more reasonable sensing performance than the sensor with PVA in Chapter 3. Therefore, in this chapter, the sensing mechanism of the sensors with Na⁺ ionic conducting material and PEI-SWNT will be discussed. This section explains the CO₂ sensing mechanism of the sensor with PEI-SWNT.

SWNT is a kind of p-type semiconductor which has been developed for the detections of various gases, such as NO₂, NH₃, H₂S, CO, SO₂ and volatile organic compounds. In this work, the polymer PEI is deposited to cover the random SWNT network to reduce the I-V hysteresis as discussed in Chapter 3. Without dopants, it is a kind of dielectric substance. The PEI molecules dispersed the nanotubes and reduced the number of the interface traps between SWNTs and oxide, and the traps inside the sensing layer. As reported in literature [53], the PEI coating can also

generate a n-type doping to the SWNTs, and result in a transition of SWNT from ptype to n-type semiconductor.

Some reports suggested that the PEI coated carbon-based materials can detect CO₂ because of the electron transportation [54]. The PEI wraps the nanotubes and changes SWNT from p-type to n-type by supplying more electrons. During the CO₂ detection, the CO₂ molecules react with PEI and affect the electron transportation in SWNTs. As a result, the resistance of SWNTs will be changed. Nevertheless, some research groups found that the CO₂ adsorption can lead to a capacitance change inside the amino functional sensing materials [55]. In reference [56], the authors proposed a capacitive CO₂ sensor by using a mixture of MWNT and SiO₂ as the sensing material. The increase of CO₂ concentration resulted in a permittivity decrease of the sensing material. Moreover, in literature [56], a mixture of 3-Aminopropyltrimethoxysilane (AMO) and Propyltrimethoxysilane (PTMS) (7:3 in volume) was used to detect CO₂ at 22°C with measuring the capacitance of the sensing material. The sensing material is filled with amino groups that can react with CO₂. The measurement results showed a decrease of capacitance when the concentration of CO₂ increased.

The branched PEI used in this work has a large amount of amino end groups inside, which are primary, secondary, and tertiary amines in a ratio of 1:1.2:0.76. All these amines can be involved in the reactions with CO₂ especially in the presence of water vapor, and form ammonium carbamate and/or ammonium bicarbonate species. The related reactions are presented as Fig. 4.1 [57]. Therefore, we suggest a hypothesis about the sensing mechanism that the change in the sensor is caused by the PEI reaction with CO₂ molecules and it is the capacitance change of the sensing material that induces the drain current change.

Fig. 4.2 shows the equivalent circuit of the sensor in (b) along A-A' in (a). The PEI-SWNT sensing material is reproduced by a series connection of a resistor R_{CG} and a capacitor C_{CG} . The C_{pass} , C_{FG} and C_p are the ONO, floating gate, and parasitic capacitances, respectively. We define γ the gate coupling coefficient between the CG and the FG. Then γ can be expressed as

$$\gamma = (C_{CG} \parallel C_{pass}) / [(C_{CG} \parallel C_{pass}) + C_p + C_{FG}]$$
(2)

During CO₂ detection, the reaction between CO₂ and the sensing material

changes the capacitance of the sensing material C_{CG} . This change will be transferred to the FG of the FET substrate through the gate coupling coefficient γ according to equation (2). As the FET substrate has a FG, the threshold voltage V_{th} relative to FG can be written as [58]

$$V_{th} = \phi_{ms} - \frac{Q_{ox}}{c_{ox}} + 2\psi_B - \frac{\sqrt{2qN_D\varepsilon_{Si}|2\psi_B|}}{c_{ox}}$$
(3)

As the *p*-MOSFET platform is used in this work, the ψ_B in equation (3) is negative, which is defined as the difference between the Fermi level and the intrinsic energy level of the silicon substrate. The ϕ_{ms} is the work-function difference between gate and Si substrate, the Q_{ox} is the equivalent oxide charge per unit area at the oxide-silicon interface, and the N_D is the doping concentration of the body. The C_{ox} equals to the C_{FG} . Consequently, the drain current of the FET substrate in the subthreshold region and linear region can be written as equation (4) and (5), respectively.

$$|I_D| = \mu C_{FG} \frac{W}{L} \sqrt{\frac{\epsilon_{\rm si} q N_{\rm d}}{4\psi_{\rm B}}} \left(\frac{kT}{q}\right) e^{q(|\gamma V_{CGS} - V_{th}|)/mkT} \tag{4}$$

$$|I_D| = \mu C_{FG} \frac{W}{L} [|\gamma V_{CGS} - V_{th}| + m V_{DS}/2] V_{DS}$$
(5)

When the concentration of CO_2 increases, the C_{CG} decreases, which

deteriorates the gate coupling coefficient γ according to equation (2). As a result, the drain current $|I_D|$ decreases according to equation (4) and (5). During the recovery of the sensor, the adsorbed CO₂ molecules will be released from the sensing material. Then the C_{CG} increases and induces the increase of coefficient γ . As a result, the drain current $|I_D|$ increases.



Fig. 4.1 Related reactions and chemical species involved in the adsorption of CO₂ by PEI. The R, R', and R" are either organic substituent of hydrogen atoms [57].



Fig. 4.2 The equivalent circuit of the sensor with PEI-SWNT. (a) The sensing material is simplified as a series connection of the R_{CG} and C_{CG} . The C_{pass} , C_{FG} and C_p are the ONO passivation, floating gate, and parasitic capacitances, respectively. (b) shows the equivalent circuit of the sensor along A-A' in (a). The γ refers to the gate coupling coefficient between the FG and CG.

4.2 Sensing mechanism of the sensor based on Na⁺ conducting material

As discussed in Chapter 2 and Chapter 3, the compound of Na₂CO₃ and NaNO₂ (the molar ratio is 1:3) is deposited on the surface of the FET sensor substrate to serve as the sensing material for the detection of CO₂ gas. According to the measurement results in Chapter 3, without APTES ionic blocking layer, Na⁺ ions can freely reach to the oxide and cause serious operating problems such as large gate leakage current and off-state current, and significant fluctuation in drain current. In contrast, with the help of APTES, the sensor can be operated as a common MOSFET and detect CO₂ gas at an appropriate working temperature. This indicates that, with the deposition process described in Chapter 2, there is a large number of mobile Na⁺ ions existing inside the sensing material. These Na⁺ ions move easily inside the sensing material and correspond to the negative fixed ions. When operating the sensor, the source is grounded and certain voltages are applied to the gate and the drain electrodes to obtain a reasonable drain current. Fig. 4.3 shows the schematic of the charge distribution within the sensor during the operation. The positive Na⁺ ions and the negative ions will distribute according to the electric field across the sensing material and affect the number of carriers in the channel of the FET [59], [60].

Fig. 4.4 shows the equivalent circuit of the sensor with Na⁺ ionic conducting material. In Fig. 4.4 (a), the sensing material is simplified as a capacitance denoted as C_{sens} [61] (including all the capacitance at the interfaces and in the bulk of the sensing material). The C_{pass}, C_{FG} and C_p are the APTES-covered ONO, floating gate, and parasitic capacitances, respectively. Note that the C_{pass} also involves the capacitance of the APTES monolayer. Fig. 4.4 (b) shows the equivalent circuit of the sensor from A to A' in (a). Appropriate V_{CG} and V_D are applied to the CG and drain electrodes, and $V_{\rm S} = 0$ V to obtain a reasonable drain current during the operation. The point B in (a) is at the interface between the sensing material and the APTES, which is corresponding to the point B in the equivalent circuit in (b). The potential drop V_{sens} resulting from C_{sens} , which is the potential difference across the sensing material (from CG to point B), is determined by the concentration of CO₂. Then, the potential at the point B in Fig. 4.4 (b), V_{CG} , can be written as

$$V_{CG}' = V_{CG} - V_{sens} \tag{6}$$

For the sensor with Na⁺ ionic conducting material, we define γ as the gate coupling coefficient relative to the point B rather than the CG metal in Fig. 4.2. In another word, the *C*_{sens} is not involved in the γ . Then the γ of the sensor with Na⁺ ionic conducting material can be represented as

$$\gamma = C_{pass} / (C_{pass} + C_p + C_{FG})$$
⁽⁷⁾

Then the voltage of the FG is

$$V_{FG} = \gamma V_{CG}' = \gamma (V_{CG} - V_{sens})$$
(8)

Therefore, when $|V_{DS}| > 2kT/q$, the drain current in subthreshold region is

$$|I_D| = \mu C_{FG} \frac{W}{L} \sqrt{\frac{\epsilon_{\rm si} q N_{\rm d}}{4\psi_{\rm B}}} \left(\frac{kT}{q}\right) e^{q(|\gamma(V_{CGS} - V_{sens}) - V_{th}|)/mkT}$$
(9)

The drain current in linear region is

$$|I_D| = \mu C_{FG} \frac{W}{L} [|\gamma (V_{CGS} - V_{sens}) - V_{th}| + m V_{DS}/2] V_{DS}$$
(10)

The V_{th} here is the same as defined in equation (3), which refers to the threshold voltage with respect to the FG.

During the gas response period, the CO_2 molecules will diffuse into the sensing material and react with Na⁺ ions. Some reports [50] suggest the involved

electrochemical reaction as

$$2Na^{+} + CO_2 + \frac{1}{2}O_2 + 2e^{-} \rightleftharpoons Na_2CO_3$$
 (11)

The mobile Na⁺ ions will be consumed by this reaction with producing neutral Na₂CO₃ molecules. In this way, the total number of Na⁺ ions are reduced, so that the distribution of Na⁺ ions inside the sensing material (C_{sens}) is changed. Then the potential difference V_{sens} across the sensing material is reduced, which results in the increase of the $|I_D|$ according to equations (9) and (10).



Fig. 4.3 Schematic of the charge distribution within the sensor during the operation.



Fig. 4.4 The equivalent circuit of the sensor with Na⁺ ionic conducting material. (a) The sensing material is simplified as a capacitor, C_{sens} . The C_{pass} , C_{FG} and C_{p} are the APTES-covered ONO, floating gate, and parasitic capacitances, respectively. (b) The equivalent circuit of the sensor from A to A' in (a).

Chapter 5

Conclusion

In this dissertation, we investigated CO₂ sensors based on FET platforms working at low temperature. Three different sensing material are developed, which are PVA polymer, PEI-SWNT random network, and Na⁺ ionic conducting material. All the materials were deposited on the surface of the FET platform by using inkjet printing process. The basic electrical and gas sensing properties of the sensors were measured. For PVA and PEI-SWNT CO₂ sensor, the working temperature is 25°C. It was found that the water vapor plays a vital role in their CO₂ detection. The sensor with PVA has short lifetime as it was degraded after 2 weeks after the deposition. By comparison, the sensor with Na⁺ ionic conducting material has the most reliable CO₂ sensing behavior. Even though the working temperature of the sensor with Na⁺ ionic conducting material is 160°C, it is still much lower than typical CO₂ sensors. In conclusion, with the help of APTES ion-blocking layer, it turns to be possible to apply the sodium ionic containing material to FET platform, and the sensor with Na⁺ ionic conducting material can be expected to promote the research on low-

temperature CO₂ sensor based on Si CMOS technology.

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초 록

지난 수십 년 동안 이산화탄소(CO₂)를 감지하고 제어하는 기술은 많 은 관심을 받아왔다. 이산화탄소의 양을 감지하는 것은 대기의 질이 어 떻게 변화하는지를 추적하는데 중요할 뿐만 아니라 관련 환경 연구에서 도 중요하다. 또한 실내공기 내의 이산화탄소는 사람에게 질병을 유발 할 수 있기 때문에 실내 이산화탄소 농도를 특정 기준 이하로 제어하는 것이 중요하다. 지금까지의 연구들은 낮은 비용, 작은 크기, 적은 전력 소비, 높은 신뢰성을 가진 CO₂ 센서를 개발하기 위해 노력하였다. 뿐만 아니라 실리콘 CMOS 센서 처리회로와 호환 가능한 센서 어례이를 만 들 수 있으며 휴대 가능한 전자 코 시스템(electronic nose system)에도 응 용할 수 있는 집적 가능한 CO₂ 센서의 수요도 증가하고 있다.

따라서 본 논문에서는 저온에서 작동하는 FET형 CO₂ 센서를 제안하 고 폴리비닐 알콜(PVA), 폴리에틸렌이민(PEI)로 코팅된 단일벽 탄소나노 튜브(SWNT), 무기 Na⁺ 이온 전도성 물질과 같은 다양한 종류의 감지 물질을 적용하였다. 감지 물질은 잉크젯 프린팅 공정을 사용하여 FET 센서 플랫폼에 증착되었다. 센서의 기본적인 전기적 특성과 CO₂ 감지 특성을 측정하였다. 이와 관련된 감지 동작 원리를 설명하고 모델링하

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였다. PVA와 PEI로 코팅된 단일벽 탄소나노튜브 CO₂ 센서는 습도의 도 움을 받아 상온(약 25°C)에서 CO₂를 검출 할 수 있다. Na⁺ 이온 전도성 물질을 가진 센서는 160°C에서 CO₂를 검출 할 수 있다. 제안된 센서는 기존의 CO₂ 센서에 비해 상대적으로 낮은 작동 온도를 갖는다. 또한 FET형 센서는 실리콘 CMOS 기술과 호환가능하다. 센서의 캘리브레이 션을 편리하게 만들기 위해 플로팅 게이트 구조를 채택하였다. 다른 감 지 물질들에 비해 Na⁺ 이온 전도성 물질을 갖는 센서는 습도의 도움을 받지 않고 감지 가능하며 가장 안정한 감지 특성을 가진다. 또한 저온 에서의 CO₂ 검출에 매우 효과적일 것으로 기대된다.

주요어: 이산화탄소 센서, FET형 센서, 낮은 온도, 폴리머, 단일벽 탄소 나노튜브, 나트륨 이온 전도성 물질.

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List of Publications

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Honors

- Young Researcher Award, The 26th Asia-Pacific Workshop on Fundamentals and Applications of Advanced Semiconductor Devices (AWAD 2018), Kitakyushu, Japan, Jul. 2018.
- Best Paper Award, 2016 Korean Sensor Society Conference, Korea, Nov. 2016.