Silver Direct Electrodeposition on Ru Thin Films

Hyo-Chol Koo,a Sung Ki Cho,a Chang Hwa Lee,b,*, Soo-Kil Kim,c,** Oh Joong Kwon,a and Jae Jeong Kima,*,†

aDepartment of Chemical and Biological Engineering, Seoul National University, Seoul 151-744, Korea
bMaterials Science and Engineering Laboratory, National Institute of Standards and Technology, Gaithersburg, Maryland 20899, USA
cFuel Cell Research Center, Korea Institute of Science and Technology (KIST), Seoul 136-791, Korea
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Ag, which has a lower resistivity and higher oxidation resistance than copper, is now regarded as the replacement for copper for the next generation interconnection material in integrated circuits.1,2 Furthermore, recent studies have suggested that the current copper damascene process, which consists of seed layer formation, bottom-up filling electrodeposition, and chemical mechanical polishing process, could easily be replaced by Ag.3-5

Ru has also been focused upon as a replacement for Ta or TiN to serve as the next generation barrier material because of its lower resistivity, good wetting property with copper,6-13 and well-established deposition processes such as chemical vapor deposition (CVD).14-15 or atomic layer deposition (ALD)16-18 that are able to produce very conformal barrier layer deposition, even at very narrow pattern sizes. The combination of Ag with a Ru barrier will have a great advantage over present materials because Ag is a noble metal that requires better glue layers in order to provide sufficient adhesion, a need that is easily met by the metallic Ru barrier.19

Direct electrodeposition is another extensively focused-upon area of research,20-22 as it will eliminate the burden of needing to form a conformal seed layer in a very narrow pattern size. Generally, direct electrodeposition on high-resistance barriers such as TiN or Ta requires a prenucleation step for the formation of continuous metal films23-25 due to the high interfacial energy between the deposited metal and substrate, which can be accomplished through Volmer-Weber nucleation.26,27 Proper prenucleation also requires surface pretreatment for the formation of continuous metal film on a heterogeneous substrate, especially in electroless plating, which is usually performed on different materials or even on dielectrics. The native oxide layers on TiN or Ta must be removed for electroless metal deposition,21 which is also necessary for the Ru barrier.22

Following surface pretreatment, the nucleation step is essential in the deposition on the heterogeneous substrate, which is more critical for the deposition of noble metals due to their usual three-dimensional nucleation with low nucleation density on a heterogeneous substrate,28 originating from their high surface energy. Previous research of direct electrodeposition has indicated that density of nucleation active sites and nucleation rate are strongly related to the applied overpotential.21,22

Because direct electrodeposition is a heterogeneous deposition process, the adhesion of a deposited film on a substrate needs to be characterized along with its effects on the electromigration resistance, which is a vital issue in metal reliability.23,27,33,35 Agglomeration, which occurs due to surface and interface diffusion, can be one of the key parameters used to estimate the adhesion and interface energy between a metal film and substrate.19,35

In the present study we focused our attention on the direct electrodeposition of Ag on Ru by optimizing surface pretreatment and nucleation steps. The thermal stability of the deposited film was tested by agglomeration at high temperature to estimate the adhesion of the film with the substrate.

Experimental

The substrate for all experiments was Ru physical vapor deposited (PVD, 50 nm)/Ta (PVD, 15 nm)/Si (PVD). For electrodeposition, a sample of the substrate was cut into a 1.5 cm square and loaded into the electrodeposition cell, which had a contact area of 1.0 cm² with the electrolyte. Except for the exposed area, all other parts of the conducting components were completely sealed using a homemade Teflon holder to avoid contact with the electrolyte. A TiN (CVD, 10 nm)/Ti (15 nm, PVD)/Si sample was used to compare the nucleation overpotential for the Ag electrodeposition using reported pretreatment methods.36 Pt wire was used as a counter electrode, and a standard calomel electrode (SCE) was used as a reference electrode. Despite that the reaction could be interfered with by the precipitation reaction between Ag⁺ and Cl⁻, the high concentration of complexing agent prevented the formation of AgCl precipitation. A standard Teflon holder to avoid contact with the electrolyte. A TiN (CVD, 10 nm)/Ti (15 nm, PVD)/Si sample was used to compare the nucleation overpotential for the Ag electrodeposition using reported pretreatment methods.36 Pt wire was used as a counter electrode, and a standard calomel electrode (SCE) was used as a reference electrode. Despite that the reaction could be interfered with by the precipitation reaction between Ag⁺ and Cl⁻, the high concentration of complexing agent prevented the formation of AgCl precipitation.

Figure 1. LSV of the Ru surface in a 0.05 M TMAH solution.
Prior to Ag electrodeposition the native oxide of Ru was electrochemically reduced in a 0.05 M tetramethylammonium hydroxide (TMAH) solution. After reduction, the sample was rinsed in deionized water without unloading from the cell. Next, the electrodeposition of Ag was performed with the electrolyte, which consisted of AgNO$_3$ (0.136 M), NH$_4$OH (0.64 M), and (NH$_4$)$_2$SO$_4$ (0.76 M).

The electrodeposition and electrochemical analysis was carried out with a Versastat II (EG&G). The measurement intervals were 0.001 s in the case of the electrodeposition, and 1 s in the case of the electrochemical reduction of Ru. Film thickness and surface morphology were measured with field emission scanning electron microscopy (FESEM, Hitachi S-4800). Crystallinity was analyzed with X-ray diffraction (XRD).

![Figure 2. AFM images of (a) Ru (no treatment), (b) oxide-reduced Ru, and their phase images (below).](image)

![Figure 3. LSV of various substrates in a Ag electrodeposition solution: (A) Ag, (B) oxide-reduced Ru, (C) Pd-activated TiN, (D) oxide-removed TiN, (E) Ru (no treatment), and (F) TiN.](image)

![Figure 4. (a) Current density profile of the Ag deposition on oxide-reduced Ru with varied applied potentials, and (b) comparison with the current transition as the applied potential in the normalized current–time form varied according to the ideal Scharifker–Hills model.](image)
The sample was annealed in a horizontal quartz tube furnace in 10 mm Hg of nitrogen ambient at 500°C. The temperature ramping rate was 16.7°C/min, and the sample was cooled to room temperature in nitrogen ambient.

Results and Discussion

The reduction was conducted in a strong basic solution of TMAH. As shown in the linear sweep voltammetry (LSV) of the Ru reduction (Fig. 1), a broad peak was observed during the initial sweep, and the peak intensity was continuously decreased as the sweep repeated. With respect to the surface reduction process, a negative potential of −0.95 V was applied for 600 s to completely remove the Ru oxide. As a result of the reduction, the surface became hydrophilic and the surface morphology became smoother according to atomic force microscopy (AFM) analysis, as shown in Fig. 2. Also, the phase image of AFM analysis showed more homogeneous material distribution after oxide reduction, which was a clue for the removal of Ru oxide. The total charge used for Ru reduction was calculated using the difference of the current from the first 600 s and subsequent 600 s of reduction with constant potential, and was determined as 7.7 mC/cm², which was comparable with the reported value of PVD Ru reduction.10

To determine the applied overpotential for Ag direct electrodeposition, the LSV of the electrodeposition solution was also performed on several substrates to compare the nucleation overpotential. As shown in Fig. 3, compared to the curve of the Ag substrate, both Ru and TiN required more than a 50 mV negative overpotential, of which the magnitude for nucleation was significantly decreased by the reduction of Ru oxide or by the formation of catalytic clusters on TiN. However, removal of Ti oxide had only a very small effect with respect to the nucleation overpotential.

Figure 4a shows the current density profiles of Ag electrodeposition on the oxide-reduced Ru substrate. As shown in the figure, the current density at the initial stage significantly increased as the applied potential decreased, which was considered as the current for nucleation. FESEM images showed that the coverage of the substrate remained low after 0.5 s of deposition. Despite the similar current density profiles of oxide-reduced Ru and TiN substrates, a continuous Ag film was not obtained on the TiN substrate even when Ag was deposited at a very negative potential for a long time. Normalization of the current with the Scharifker–Hills model37 (Fig. 4b) showed that all of the curves deviated from the ideal nucleation model. Every case, regardless of the applied potential, exhibited a larger current density than the ideal instantaneous nucleation model;
such deviation may have been due to charge-transfer governing
growth or nonideal nucleation, which made deviations from the
assumption of the ideal model. In this case, the early coalescence
of Ag particles observed prior to the complete covering of the substrate
as well as formation of abnormally large Ag particles might be pos-
sible reasons for the deviation. Furthermore, a strong negative po-
tential may induce the hydrogen evolution simultaneously. However,
the precise effects of these factors are not clear.

The effect of oxide reduction on the initial stage deposition with
various applied potentials is shown in Fig. 5. There were obvious
decreases in the nucleation density with a more positive applied
potential after 0.1 s of deposition; however, the difference in nuclea-
tion density was not notable below −0.8 V when oxide reduction
was employed, whereas the increase of the nucleation density was
obvious without oxide reduction. There were slight increases in cur-
rent density by oxide reduction, but formation of a continuous Ag
film was not possible without the oxide reduction shown in Fig. 6.

Figure 7 shows the surface morphology of various Ag films de-
posited on the oxide-reduced Ru substrate. Some voids were incor-
porated into Ag films that were deposited at more positive potent-
ials, as in the case of the 60 nm Ag film, which may have resulted
from a low nucleation density. For 90 nm thick Ag films, the surface
morphologies of all cases were comparable to each other, regardless
of the applied potential.

The values of resistivity of the 90 nm films were in the range of
2.6–2.8 μΩ cm (Fig. 8a). The 60 nm Ag films had a slightly higher
resistivity and slightly larger deviation as the applied potential be-
came more positive. As shown in Fig. 8b, there is a clear Ag(111)
peak. Careful consideration of peak overlap between Ag and Ru
must be included. The XRD data of only the Ru film revealed that
the strong peak near 44° is almost Ru(101). There was also a slight
overlap between the Ag(111) and Ru(100) peaks. The grain size
from the Scherrer equation was calculated to be about 25 nm, which
was smaller than the previously reported mean-free path of electrons
in Ag.

Thermal stability of the 60 nm film was tested by annealing at
500°C for several hours in nitrogen ambient. As shown in Fig. 9,
while the extent of agglomeration was considerably affected by the
applied potential, the final state of agglomeration remained the same
regardless of applied potential. The sheet resistance changes noted
in Fig. 10 provided more quantitative data regarding the extent of
agglomeration. Higher negative potentials reduced the accelerating
rate of sheet resistance. Interestingly, with thicker films, the sheet
resistance was slightly decreased, even after 4 h of annealing, as
shown in Fig. 11. This phenomenon may be due to the different ratio
between the interface and the total volume of the film.

In this study, we found that oxide reduction of Ru was a critical
factor for the formation of a continuous Ag film and that the applied
potential affected the initial nucleation stage and the thermal stabil-
ity of the film. The link between these two findings was not initially
clear. As reported in previous research, the nucleation density at the
initial stage is strongly affected by the applied potential, and this
may be the reason for the limited kinetic stability observed during
agglomeration. The film adhesion and chemical interaction between
film and substrate are presumably linked to the nuclei formed at the
initial stage. After the formation of nuclei, growth of Ag proceeds
from the Ag nuclei, not the substrate, due to the large difference in
nucleation overpotential. Better adhesion and dense chemical inter-

![Figure 8](image_url)

**Figure 8.** (a) Resistivity of the Ag films as film thickness and applied po-
tential were varied, and (b) crystallinity of the Ag films (60 nm) as the
applied potential was varied.

![Figure 9](image_url)

**Figure 9.** Surface morphology of the 60
nm thick Ag films after annealing at
500°C in nitrogen ambient.
action spots might be the origin of better agglomeration resistance, due to the slower interfacial diffusion of Ag atoms at the interface. Addition of a suppressor was also employed to enhance nucleation. For the direct electrodeposition of Cu on Ru, addition of the suppressor PEG-Cl\(^-\) results in increased nucleation density.\(^{39}\) In this study, 3-amino-1,2,4-triazole, which has a similar structure to other Cu corrosion inhibitors such as benzotriazole or 5-aminotetrazole, was added to the electrolyte in order to suppress further growth.\(^{40}\) The addition of 3-amino-1,2,4-triazole strongly enhanced nucleation density and considerably improved the coverage of 0.1 s into deposition compared to cases without suppressor.\(^{41}\) The LSV data in Fig. 13 showed that the addition of the suppressor slightly increased the overpotential for nucleation on both electrodes, but also decreased the difference of overpotential between electrodes, which was interpreted as a lower energy barrier for the nucleation, leading to a higher population.\(^{41}\) In addition, it was suggested that the preferential adsorption of suppressors on the growing Ag clusters inhibited local growth acceleration of the early stage nuclei. Therefore, when the suppressor was added to the electrolyte, a continuous growth of Ag film on the already-formed Ag cluster was suppressed and new cluster formation was able to begin. The higher nucleation density at the initial stage also induced better adhesion to the substrate and enhanced thermal stability.

**Conclusion**

Direct electrodeposition of Ag was performed on Ru thin film following electrochemical reduction of Ru oxide. At higher negative potentials the current density during the initial stage increased significantly and nucleation density was enhanced. Even though the nucleation profile was not significantly different between reduced and nonreduced Ru oxide, we found that the oxide reduction was a critical process for the formation of a continuous Ag thin film. The applied potential also affected the extent of agglomeration. Even though there were no significant differences in the final breakdown of the metal films, the increased rate of sheet resistance and altered surface morphology was strongly suppressed with a more negative potential. A higher nucleation density at the initial stage was closely related with better resistance to agglomeration. The nucleation density was also increased by the addition of a suppressor, which decreased the difference between the nucleation overpotential on Ag and Ru.

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Figure 13. (a) LSV of the electroplating solution after addition of the suppressor and substrate material, and (b) a magnified section near the equilibrium potentials.

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References